

Robust Stability

MEM 355 Performance Enhancement of Dynamical Systems

Harry G. Kwatny
Department of Mechanical Engineering & Mechanics
Drexel University

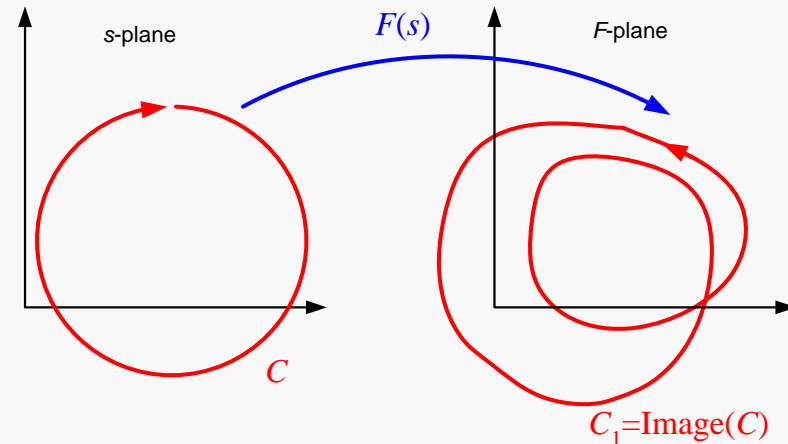
Outline

- **Stability & Robustness**
- **Introduction – role of sensitivity functions**
- **Nyquist Analysis**
- **Traditional gain/phase margins**

Introduction to Nyquist Stability Analysis

- Nyquist Analysis
 - A graphical method to determine how many closed loop poles are in the right half plane
 - Developed in the early 1930's – those days it was not easy to find the roots of high order polynomials
- Stability Margins
 - Nyquist analysis provides a clear concept of 'stability margin'
 - This concept generalizes to more complex MIMO systems
 - It remains a key concept in the current era

Cauchy Theorem



Any function of a complex number can be viewed as a map of points in one complex plane to another

Theorem (Cauchy): Let C be a simple closed curve in the s -plane. $F(s)$ is a rational function, having neither poles nor zeros on C . If C_1 is the image of C under the map $F(s)$, then

$$Z = P - N$$

where

N the number of **counterclockwise** encirclements of the origin by C_1 as s traverses C once in the **clockwise** direction.

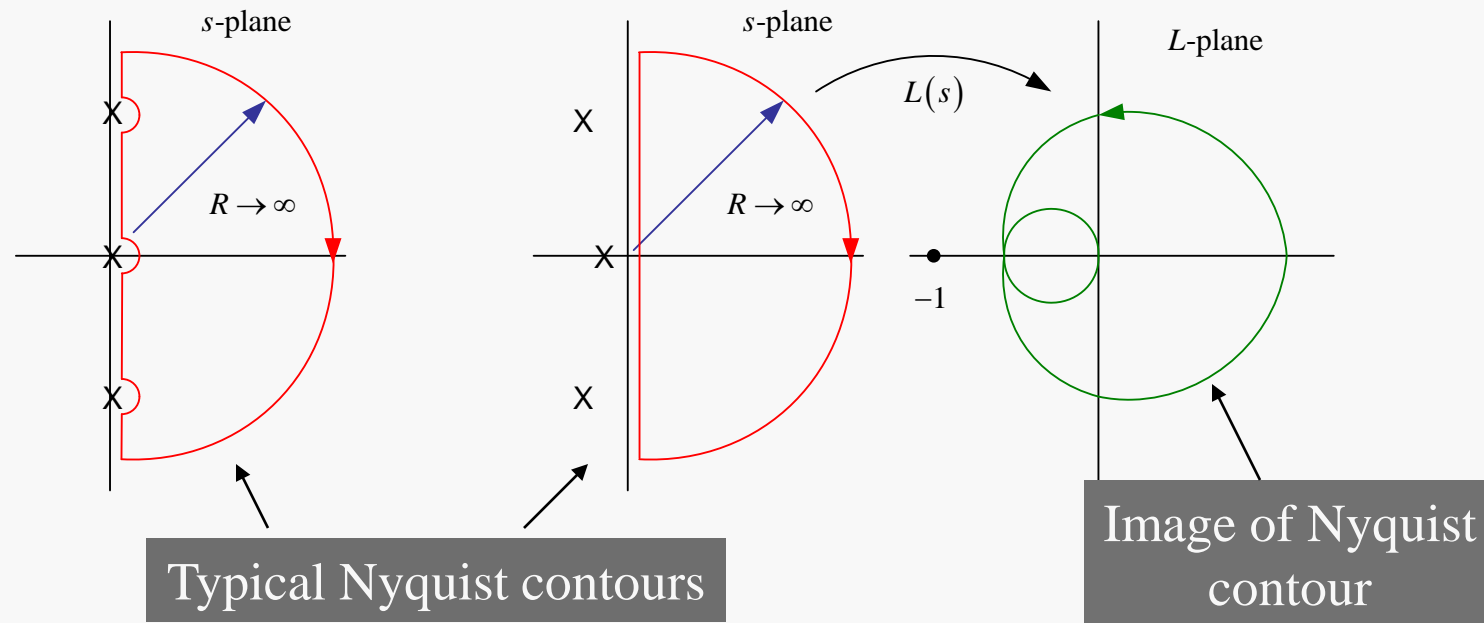
Z the number of zeros of $F(s)$ enclosed by C , counting multiplicities.

P the number of poles of $F(s)$ enclosed by C , counting multiplicities.

Nyquist

S, Sensitivity function

- Take $F(s)=1+L(s)$ (note: $F=S^{-1}$)
- Choose a C that encloses the entire RHP
- Map into L -plane instead of F -plane (shift by -1)



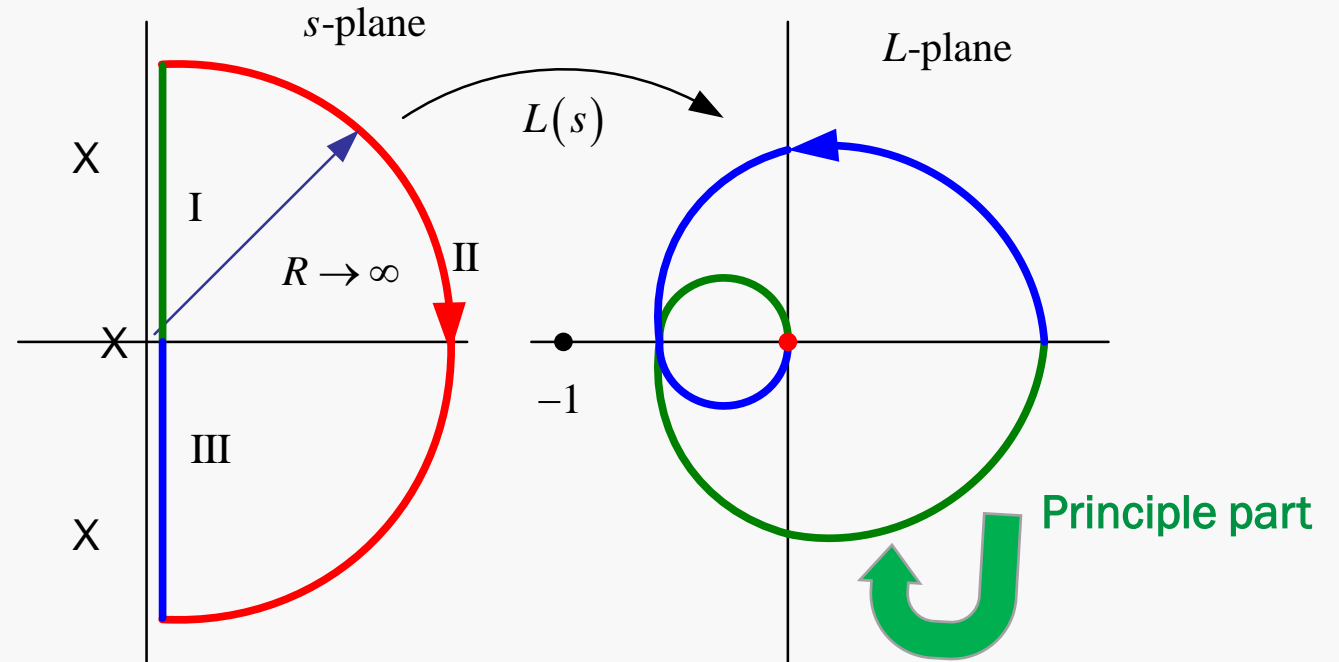
Nyquist Theorem

Theorem (Nyquist): If the plot of $L(s)$ (i.e., the image of the Nyquist contour in the L -plane) encircles the point $-1+j0$ in the counterclockwise direction as many times as there are unstable open loop poles (poles of $L(s)$ within the Nyquist contour) then the feedback system has no poles in the RHP.

$$Z = P - N$$

closed loop poles in RHP = open loop poles in RHP - cc encirclements of -1

Example 1



$$L(s) = \frac{1}{(s + p_1)(s^2 + 2\zeta\omega_0 s + \omega_0^2)}$$

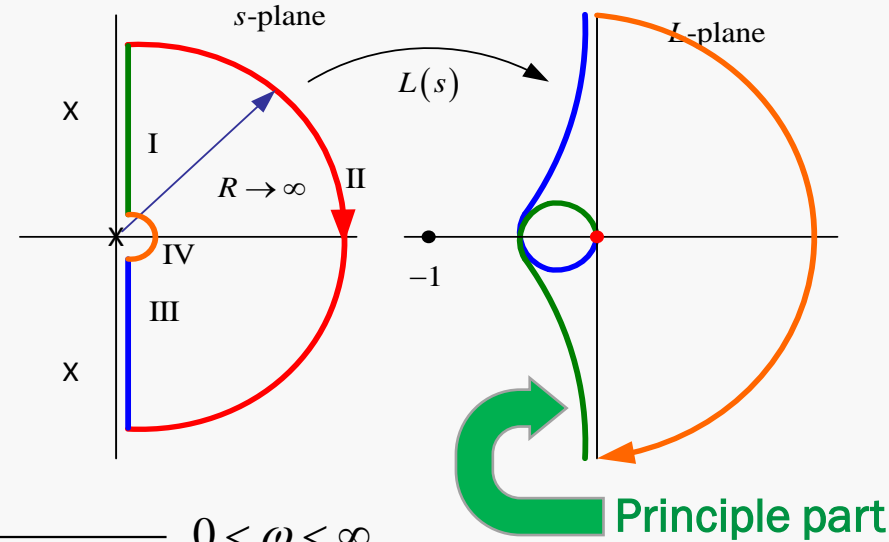
$$\text{I: } s = j\omega \Rightarrow L(j\omega) = \frac{1}{(j\omega + p_1)(-\omega^2 + 2\zeta\omega_0 j\omega + \omega_0^2)}, 0 < \omega < \infty$$

$$\text{II: } s = \rho e^{j\theta}, \rho \rightarrow \infty, = \frac{\pi}{2} \downarrow -\frac{\pi}{2}$$

$$L(\rho e^{j\theta}) = \frac{1}{(\rho e^{j\theta} + p_1)(\rho^2 e^{j2\theta} + 2\zeta\omega_0 \rho e^{j\theta} + \omega_0^2)} \xrightarrow{\rho \rightarrow \infty} 0$$

$$\text{III: } s = -j\omega, \text{ III} \rightarrow \text{I}^*$$

Example 2



$$L(s) = \frac{1}{s(s^2 + 2\zeta\omega_0 s + \omega_0^2)}$$

$$\text{I: } s = j\omega \Rightarrow L(j\omega) = \frac{1}{j\omega(-\omega^2 + j2\zeta\omega_0\omega + \omega_0^2)}, 0 < \omega < \infty$$

$$\text{II: } s = \rho e^{j\theta}, \rho \rightarrow \infty, \theta = \frac{\pi}{2} \downarrow -\frac{\pi}{2}$$

$$L(\rho e^{j\theta}) = \frac{1}{\rho e^{j\theta} (\rho^2 e^{j2\theta} + 2\zeta\omega_0 \rho e^{j\theta} + \omega_0^2)} \xrightarrow{\rho \rightarrow \infty} 0$$

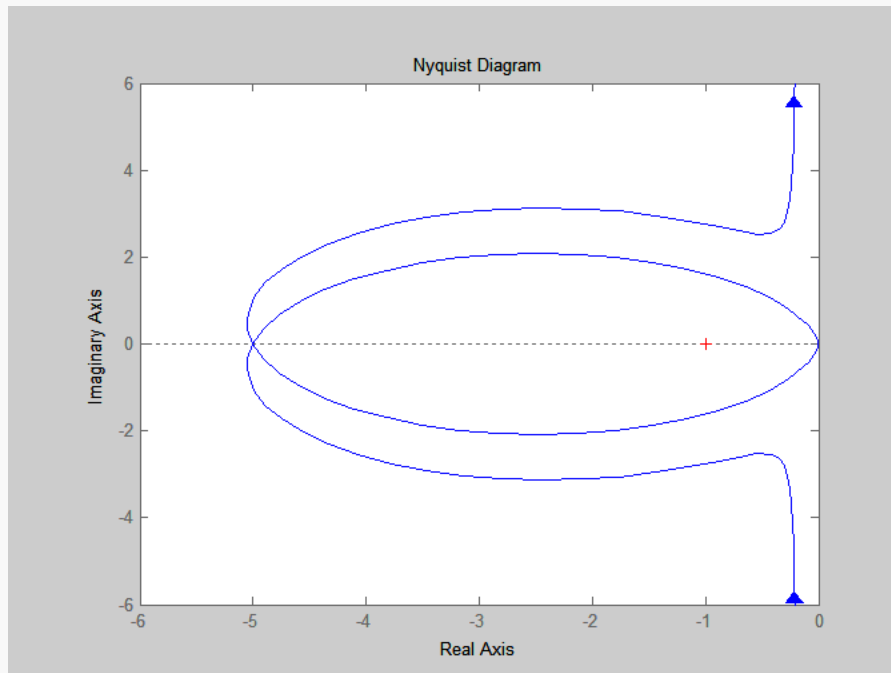
$$\text{III: } s = -j\omega, \text{ III} \rightarrow \text{I}^*$$

$$\text{IV: } s = \varepsilon e^{j\theta}, \varepsilon \rightarrow 0, \theta = -\frac{\pi}{2} \uparrow \frac{\pi}{2}$$

$$L(\varepsilon e^{j\theta}) = \frac{1}{\varepsilon e^{j\theta} (\varepsilon^2 e^{j2\theta} + 2\zeta\omega_0 \varepsilon e^{j\theta} + \omega_0^2)} \xrightarrow{\varepsilon \rightarrow 0} \frac{1}{\varepsilon \omega_0^2} e^{-j\theta}$$

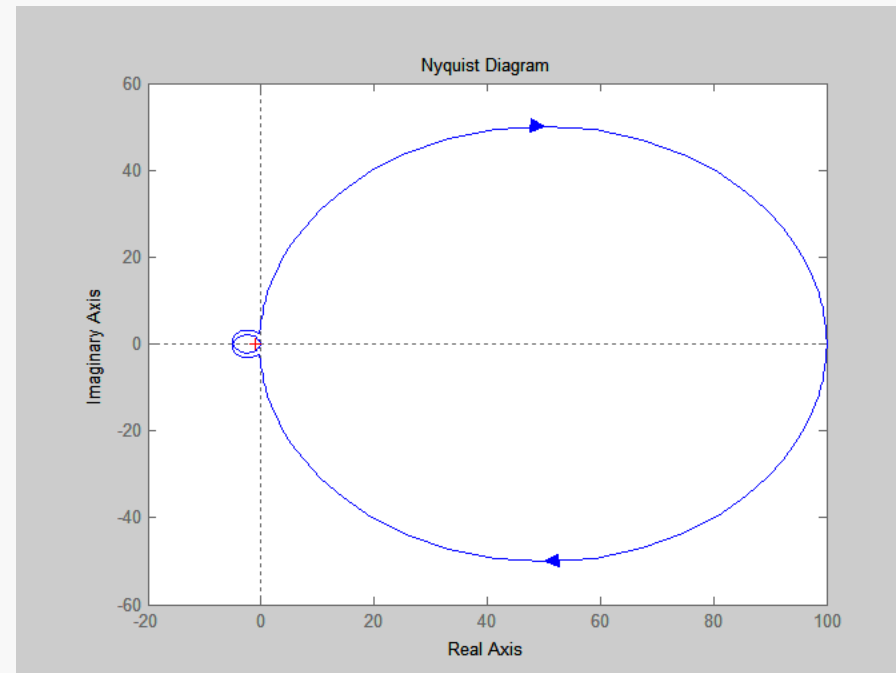
Example 3

```
>> s=tf('s');  
>> G=1/(s*(s^2+2*0.1*s+1));  
>> nyquist(G)
```



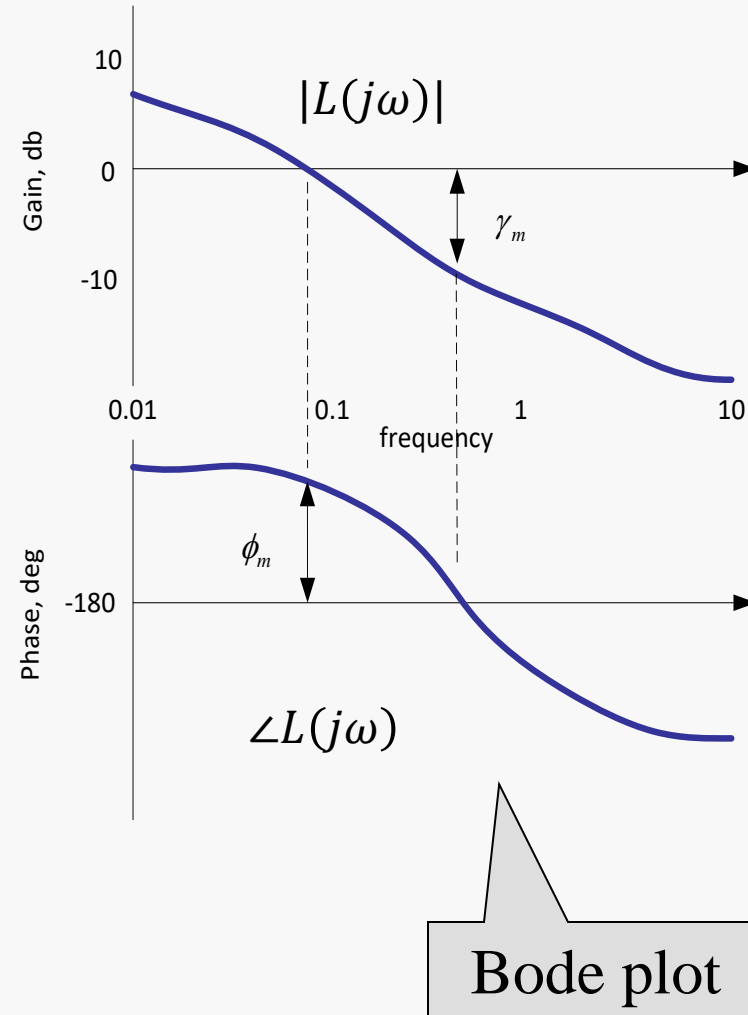
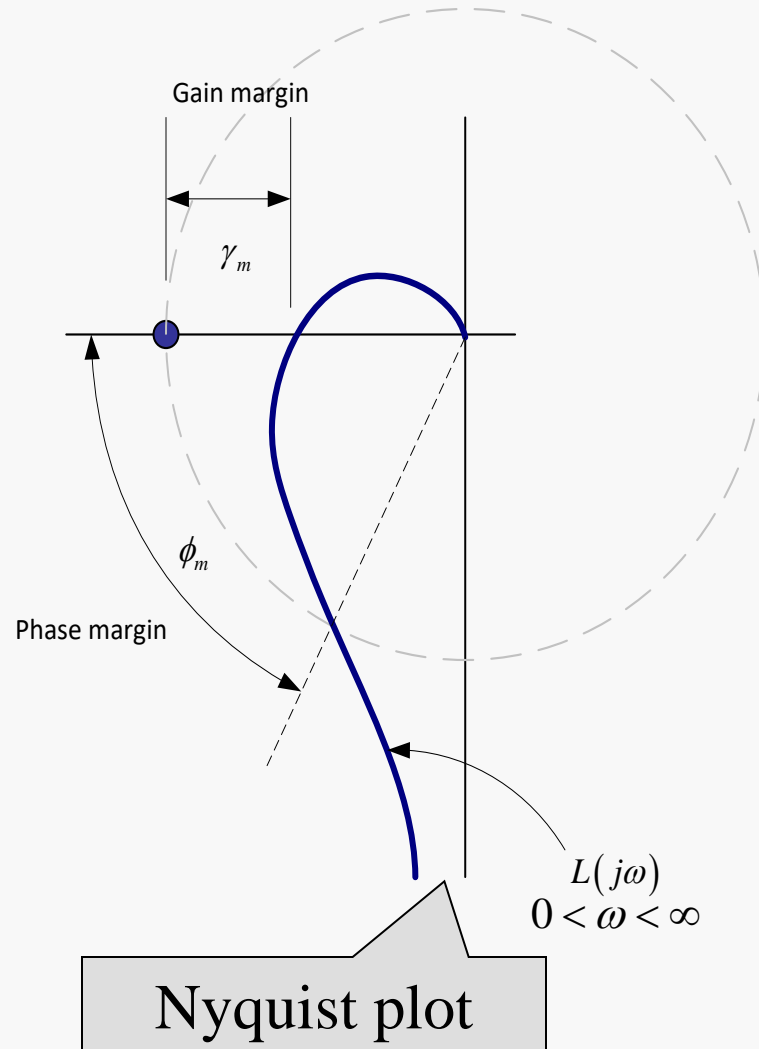
$$G(s) = \frac{1}{s(s^2 + 2(0.1)s + 1)}$$

```
>> s=tf('s');  
>> G=1/((s+0.01)*(s^2+2*0.1*s+1));  
>> nyquist(G)
```



To
obtain
global
picture

Gain & Phase Margin



Robustness From Sensitivity Functions

Sensitivity peaks are related to gain and phase margin.

Sensitivity peaks are related to overshoot and damping ratio.

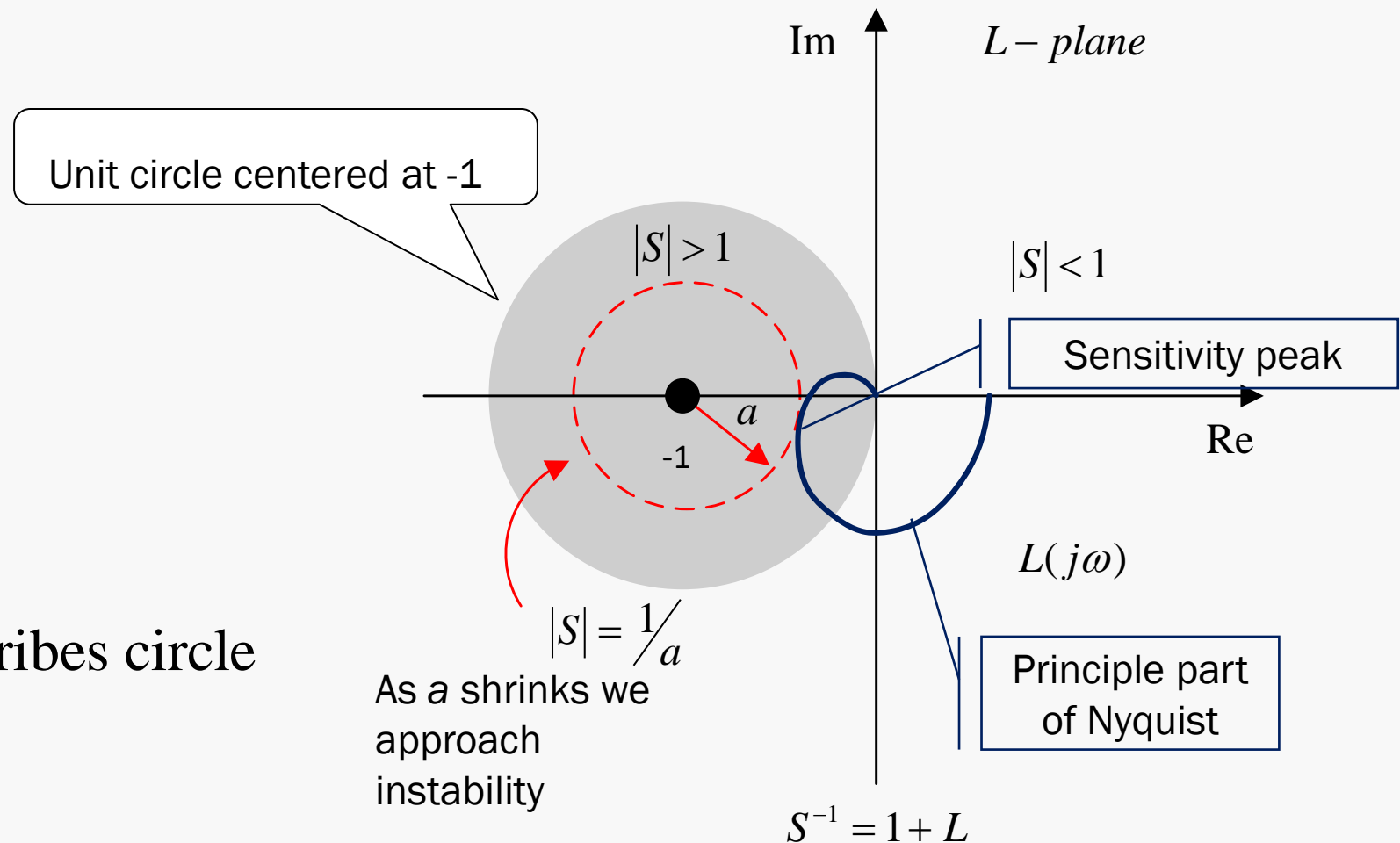
$$M_S = \max_{\omega} |S(j\omega)|$$

$$M_T = \max_{\omega} |T(j\omega)|$$

$$S = \rho e^{j\theta} = (1 + L)^{-1}$$

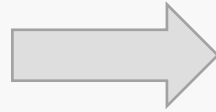
$$\Rightarrow L = -1 + \rho^{-1} e^{-j\theta}$$

constant $|S|$ prescribes circle

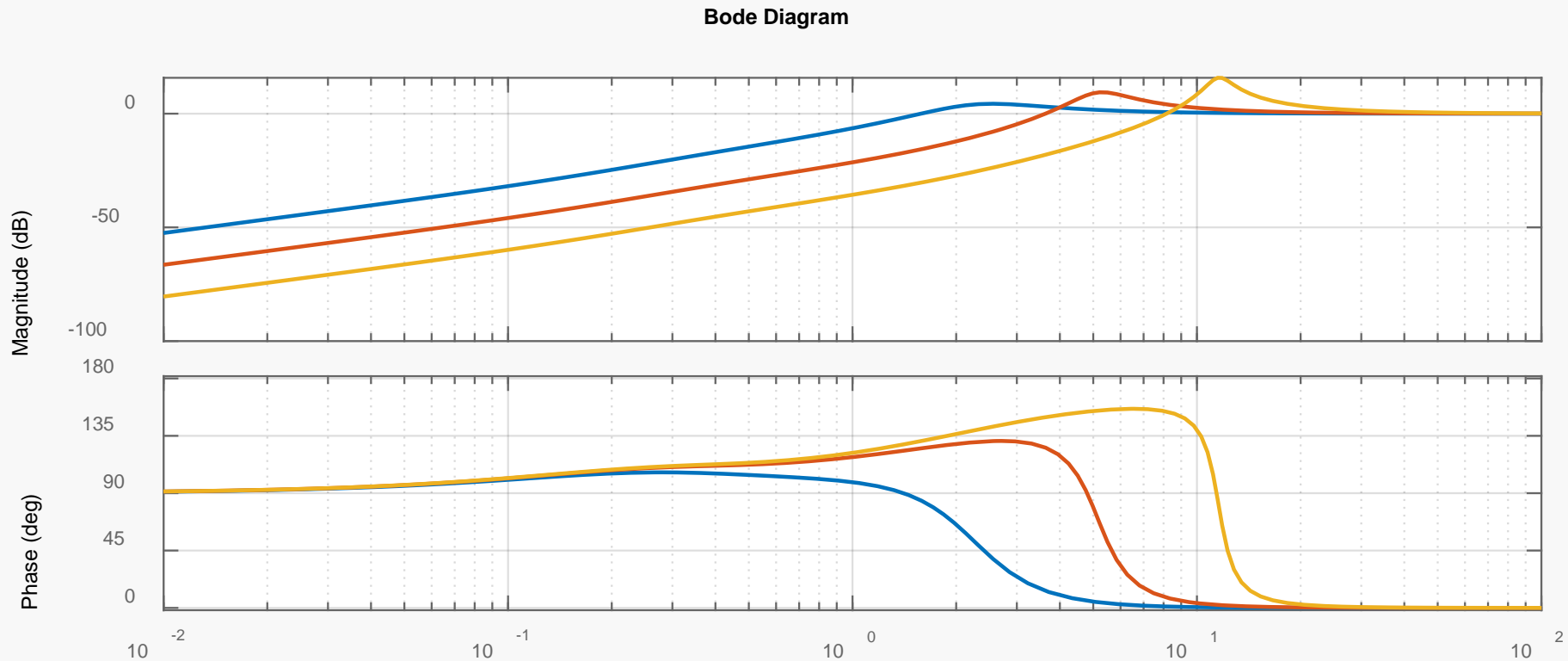


Example: XV-15

Sensitivity function plots for $K=1, 5, 25$

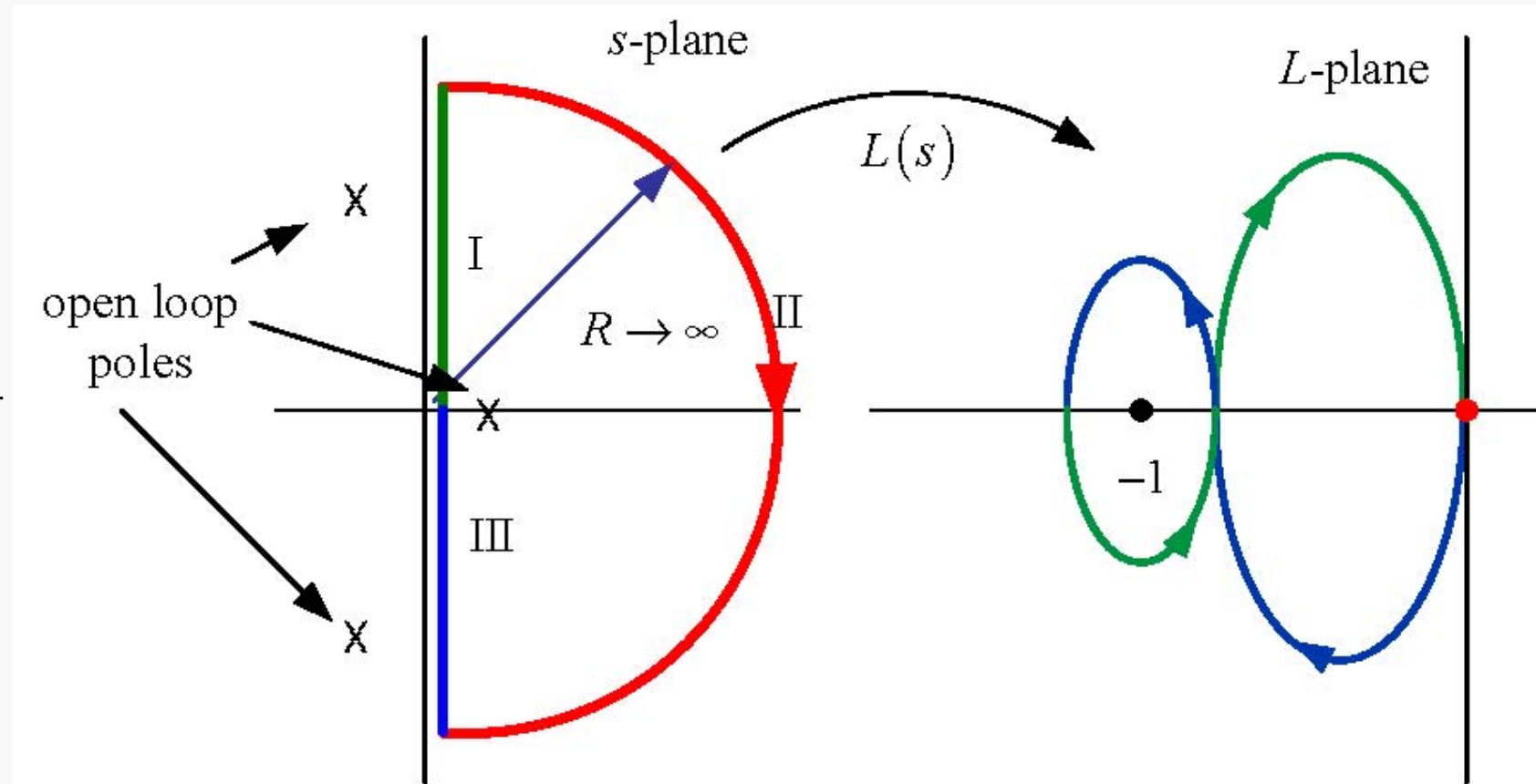


Larger sensitivity peak, closer to instability, reduced gain and phase margins, reduced damping, increased overshoot



Example: single unstable pole

$$L(s) = \frac{1}{(s - p_1)(s^2 + 2\rho\omega_0 + \omega_0^2)}$$



Example Cont'd- MATLAB Computations

$$L(s) = \frac{0.6}{(s-0.5)(s^2+s+1)}$$

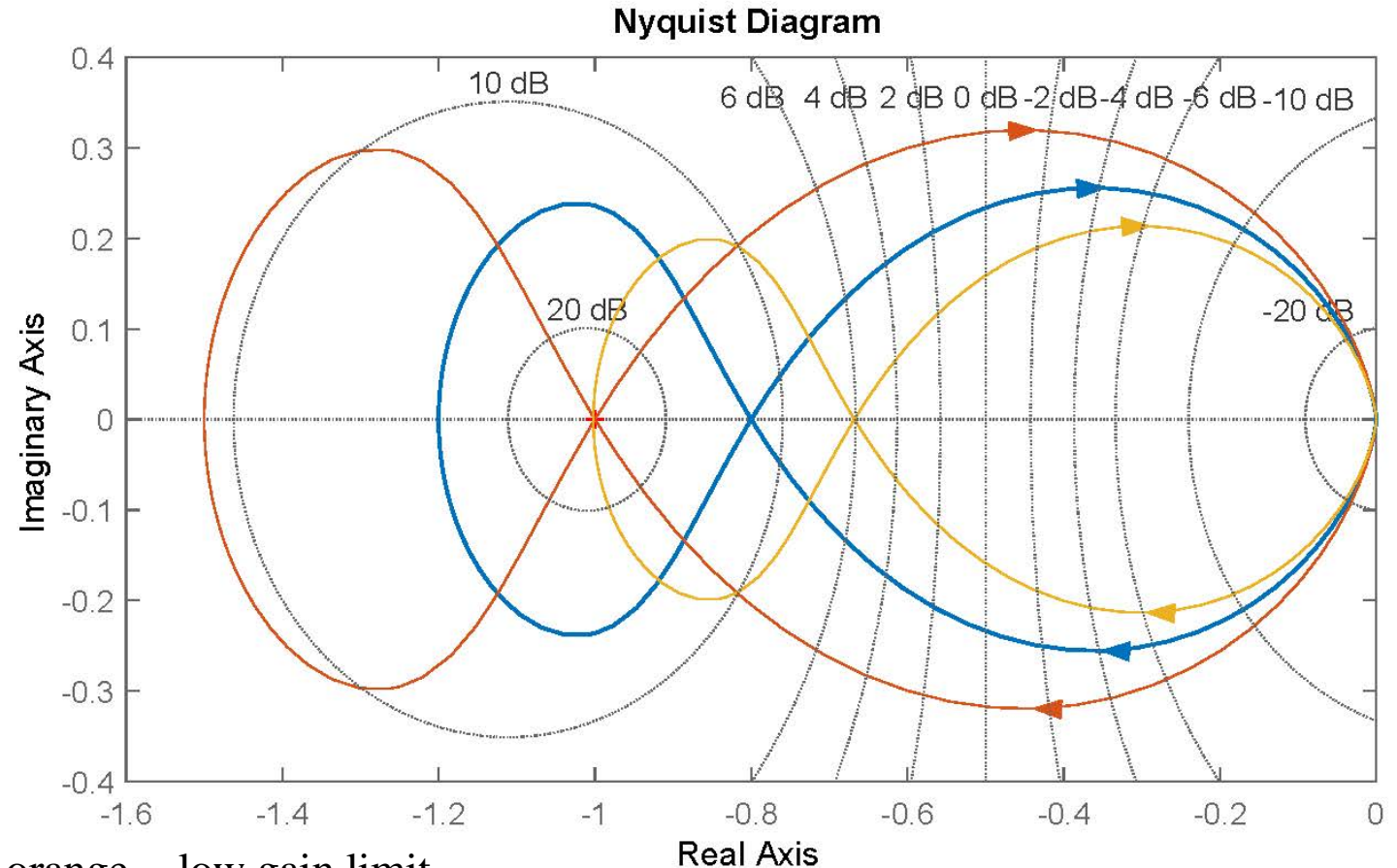
`s=tf('s')`

`L=0.60/((s-0.5)*(s^2+s+1));`

`figure`

`nyquist(L,1.25*L,0.835*L)`

`grid`



$0.835L(s)$	orange	low gain limit
$L(s)$	blue	stable
$1.25L(s)$	red	high gain limit

Summary

- Need to consider 2-3 transfer functions to fully evaluate performance
- Bandwidth is inversely related to settling time
- Sensitivity function peak is related to overshoot and inversely to damping ratio
- Gain and phase margins can be determined from Nyquist or Bode plots
- Sensitivity peak is inversely related to stability margin
- Design tools:
 - Bode and/or Nyquist diagrams helps establish robustness (margins) & performance (sensitivity peaks)